

## SECTION 5

# The Experimental Data Validation of Modern Newtonian Gravitation

### 1 – INTRODUCTION AND SUMMARY

The theory of gravitation presented by General Relativity [GR], although highly successful at treating phenomena resulting from gravitation, fails to obtain precise measurement of *Big G*, the Newtonian constant of gravitation, has failed to connect *Big G* to the rest of physic's fundamental constants, proffers no cause or mechanism for the operation of gravitation, and consequently prevents any development of means of controlling or modifying gravitation.

The Modern Newtonian [MN] theory of gravitation overcomes all of those GR failures.

The difference between the two theories is in the interpretation of Newton's formula for gravitational action, 4-1 below, specifically the interpretation of the  $1/d^2$ .

$$(5-1) \quad a_g = G \cdot \frac{M}{d^2} \quad F = G \cdot \frac{M \cdot m}{d^2}$$

In GR the separation distance,  $d$ , between the gravitating objects' masses,  $M$  and  $m$ , is the distance between the centers of the two.

In MN each of the objects is composed of myriad particles, atoms, each of which performs equation 4-1 between itself and each of the particles in the other object, individually, one-on-one as an independent pair. Each such pair has its particular separation distance. The inverse separation distance squared,  $1/d^2$ , of equation 4-1 is the overall average of the myriad individual inverse separation distances squared, corrected to the vector component parallel to the centerline between the objects,  $Avg[1/d^2]$ .

To convert a measurement of *Big G* done using the GR version of equation 4-1 to the value that would have been obtained if the measurement had been done using the MN version of equation 4-1 it is only necessary to multiply the GR version measurement by the GR inverse separation distance squared,  $1/d^2$ , divided by the MN average of the squared inverse separation distances,  $Avg[1/d^2]$ .

The just prior Section 4, “Connecting Newton’s G With the Rest of Physics” presents a formula for calculating *Big G* from other fundamental physics constants. From that the correct value of *Big G* is  $6.636,046,823 \times 10^{-11} m^3 kg^{-1} s^{-2}$ . In converting GR *Big G* measurements to MN the GR are not precise due to their various measurement errors so that those converted to MN per the above procedure will not arrive at the above precise *Big G* from fundamental constants but will deviate because their other measurement errors will still be present.

The results of some such conversions, from GR to MN, are presented in Table I, below. Note the variations in the “Corrected” values around the “*Big G* from fundamental constants”  $6.636,046,823 \times 10^{-11}$  value. The variations in the “Corrected” are caused by the original measurements’ variations.

TABLE I – SUMMARY OF TESTS RESULTS

All Data in SI Units: meters, kilograms, seconds \* =  $\times 10^{-11}$

Measurement	Description of Experiment	Year	GR 1/D <sup>2</sup>	MN AvgD	Gm as * Measured	Corrected G *
Correct = 6.636,046,823						
Cavendish	Sphere on sphere torsion balance, deflection	1798	18.90	20.355,903,3	6.754	6.272
Rose	Sphere on cylinder, off-set by angular acceleration	1969	33.029,464,1	33.243,545,7	6.674	6.631
Luther	Sphere on torsion pendulum, oscillation frequency	1982	202.359,259,3	203.647,993,0	6.672,6	6.630,4
Bagley 1	Sphere on torsion pendulum, time-of-swing	1997	193.388,696,3	194.648,677,3	6.676,1	6.632,8
Bagley 2	Sphere on torsion pendulum, time-of-swing	1997	204.919,773,9	206.216,007,9	6.678,4	6.636,4
Gundlach	Sphere on cylinder, off-set by angular acceleration	2000	15.081,535,4	15.178,361,1	6.674,215	6.631,639
Schlamminger	A Configuration of Cylinders, beam balance	2006	20.020,909,8	20.149,705,7	6.674,252	6.631,591
Quinn	Cylinders torsion pendulum, average of fixed deflection and period of oscillation	2013	0.138,195,9	0.139,108,2	6.675,66	6.631,67

The conclusion is that the Section 4 derivation and its formulation for *Big G* in terms of other fundamental physics constants is valid and correct. That which GR could not produce has been produced and resolved by MN gravitation which consequently must supersede GR gravitation.

Further, this MN validation also “legitimizes” the *Gravito-Electric Power Generation* and the *Gravitation Deflector Spacecraft Deep Space Drive* and the *Gravitation Deflector Planet Surface Flying Vehicle* proposals in the further below Section 8, “Gravitational and Anti-Gravitational Applications” which applications should be pursued.

**II – ON THE THEORY OF MEASURING BIG G**

There is only one universal correct value of *Big G*. Except for various errors and inaccuracies in conducting the measurement every measurement must provide that exact same result. While the gravitational acceleration or force acting between objects varies according to Newton’s Law that variation is due to varying values of the masses involved and the separation distance not the value of *Big G* which is a fixed constant.

But, in the MN conception of the operation of Newton’s Law the separation distance is not the simple distance between the centers of the two gravitating masses; it is the average of the inverse square separations particle to particle, one on one, of all of the particles making up the masses. Therefore different configurations of the gravitating masses produce different gravitational acceleration and force for the same GR values of the masses with the same GR center to center separations.

Nevertheless, whatever the values of the masses are and whatever the configuration of their particles and whatever the resulting gravitational acceleration and force, the measurement of *Big G* must produce the same universal value. Any deviations or discrepancies from the correct value can only be due to measurement errors and inaccuracies.

Consider two measurement alternatives both having the same masses acting and the same GR separation distance between the centers of those masses, but the configurations of the MN interacting particles making up the masses are different. For example, alternative #1 is two spheres whereas alternative #2 is two cylinders.

It might be thought that the measured gravitational acceleration or force would be the same for the two alternatives because in the GR conception of Newton’s Law of Gravitation the two alternatives are identical, not a little different. But regardless of the GR thinking, the actual measurements will be different because it is the MN gravitational action that operates, always.

The MN average inverse square separation,  $Avg[1/d^2]$ , in the two alternatives must be at least a little different. The MN difference in the two alternatives will produce accordingly different resulting gravitational acceleration or force which will result in accordingly different values for *Big G* calculated by GR.

The formula for correcting those GR values of *Big G* to the MN values for the two alternatives results in the same value for *Big G* always.

$$\begin{aligned} \text{Correct } Big\ G = & \frac{\text{Spheres GR Measured } Big\ G \text{ Unknowingly Using}}{\text{Spheres MN Particles Action}} \times \frac{\text{GR Inverse Square Separation}}{\text{Spheres MN } Avg[1/d^2]} \\ \text{Correct } Big\ G = & \frac{\text{Cylinders GR Measured } Big\ G \text{ Unknowingly Using}}{\text{Cylinders MN Particles Action}} \times \frac{\text{GR Inverse Square Separation}}{\text{Cylinders MN } Avg[1/d^2]} \end{aligned}$$

In both alternatives the formula cancels out the GR  $1/d^2$  [used to calculate *Big G* from the actually measured gravitational acceleration or force observed] replacing it with the  $[Avg[1/d^2]]$  that was actually operating when the measurement was made.

The problem in making this correction is to accurately calculate  $Avg[1/d^2]$ , that is to exactly reproduce the particle-by-particle, particle-to-particle, one-on-one action that actually operates in the Newtonian gravitational interaction, that actually operated in each experimental result to be converted.

III – THE POINT-ON-POINT GRAVITATIONAL INTERACTION BETWEEN OBJECTS

In this *Big G* Calculation, each of the particles in *M* is paired, one at a time, with every particle in *m*. The particle-to-particle separation distance in their 3-dimensional space is determined from the 3-dimensional Law of Pythagoras. That distance is then squared and its reciprocal taken producing the equivalent of gravitation’s  $1/d^2$ . corresponding to the contribution to  $F_{grav}$  of the particular particle pair of one particle of *M* interacting with one particle of *m*. The components of this gravitational action that are perpendicular to the center-to-center line have no net effect because over all of the particle-to-particle interactions and the symmetry of the configuration they cancel out. Only the component of the gravitational action between two particles that is parallel to the center-to-center line is effective gravitation. That component is evaluated by projecting the 3-dimensional line of each particle-to-particle interaction onto the center-to-center line.

The average of the accumulation of all of these [MN] particle-to-particle results is then compared to the corresponding [GR] center-to-center results.

This calculation is part of the calculating of the particle-on-particle interactions between the particles of a “source” gravitating object and the “encountered” gravitating object the particles represented by approximating samples [dealing with “points” is impossible; there are an infinite number]. The objects are deemed monolithic solids of purely one kind of particle. The particles are expressed in terms of a set of 3 - dimensioning axes: *x*, *y*, and *z*.

The origin of those coordinates is at the center of the source object. The coordinates are *x<sub>s</sub>*, *y<sub>s</sub>*, and *z<sub>s</sub>* designating individual points in the source object.

For the purpose of referring to particles in the encountered object a secondary origin is taken at the center of that object and the coordinates there are *x<sub>e</sub>*, *y<sub>e</sub>*, and *z<sub>e</sub>*.

The center-to-center (origin-to-origin) separation distance of the two objects is the distance  $D$ . In terms of source dimensioning the origin of the encountered object is located at  $x_s = -D$ . Any encountered coordinate designation is referred to the source dimensioning by adding “ $-D$ ” to the  $x_e$  dimension.

The total particle-on-particle interaction is obtained by summing the individual contributions of each source point interacting with each encountered point. The scanning process selects successive values of  $z_s$ , each value representing a 2-dimensional “slice” of the source object. The slice is then scanned into successive values of  $y_s$  representing 1-dimensional lines making up the slice. Each line is then scanned into successive values of  $x_s$  representing 0-dimensional points making up the line.

Each of those source points then interacts with each of the points of the encountered object selected by the same slice - line - point type of scanning process as used for the source object. When the currently selected source point  $i$ , which is  $z_{s_i}, y_{s_i}, x_{s_i}$ , has interacted with every one of the encountered object points successively one at a time then the scan proceeds to source point  $(i + 1)$  and its interaction with every one of the encountered object points.

The entire process is extremely lengthy. To shorten it, which corresponds to speeding it up, the portion of the process that is most used, the  $x_e$  scan, is replaced by developing a formula that gives the same result as the  $x_e$  scan it replaces. This procedure has two advantages, the first being that calculating the effect of an entire line of points “in one fell swoop” is much faster than calculating that entire line one point at a time.

The second advantage is as follows. There are an infinite number of points in a line and they cannot be individually addressed. Rather the line must be divided into a number of sequential identical segments they being samples of the line. The more segments the line is represented by the greater the precision of the samples accurately representing the line. The replacement of  $x_e$  sampling with “one fell swoop” calculation also produces the maximum precision.

The same necessity for sampling applies to the succession of lines as the  $y_e$ -variable progresses and to the succession of “slices” as the  $z_e$ -variable progresses. Therefore each sample “point” is actually a sample volume, a *cuboid* (or *rectangular parallelepiped*) of which the “point” is the location of the *cuboid* center and which *cuboids* all taken together are the volume of the object.

A spherical quadrant is each of four parts of a sphere divided by two planes at right angles to each other. In the present 3-dimensional  $x, y, z$  coordinate system let the two planes be the  $x$ - $y$  plane and the  $x$ - $z$  plane as in the left Figure below. Taking advantage of the symmetry of the two spheres addressing each other along a line connecting their centers as in the right Figure below, that center line their common  $x$ -axis, each sphere has four such quadrants and if the entire source sphere is scanned then, because of the symmetry, each of the encountered sphere’s four quadrants produces the same effect and only one of them need be scanned.

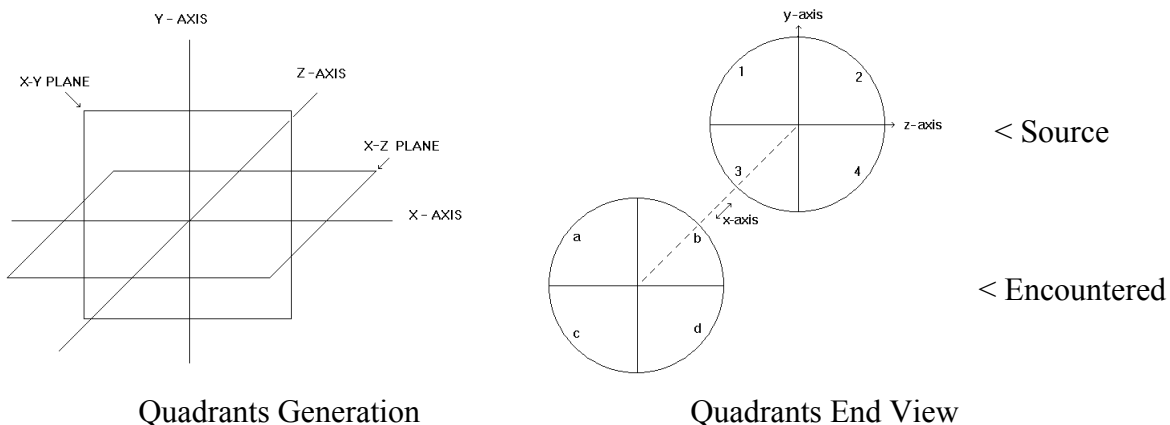


Figure 4-1

Furthermore, the source sphere need be scanned in only one of its four quadrants, that involving  $+ys$  and  $+zs$  the other three quadrants then being selected by successively choosing  $-ys$  with  $+zs$ ,  $-ys$  with  $-zs$ , and  $+ys$  with  $-zs$ .

Finally because of the symmetry the interaction of  $Q1$  with  $Qb$  is the same as  $Q1$  with  $Qc$  so that only one of those two need be calculated, the result of that being doubled.

The  $x_e$  scan is for one single point of the source sphere, that is one single set of values for  $xs$ ,  $ys$ , and  $zs$ . It is for one single line parallel to the x-axis, that line for one single set of values of  $ye$  and  $ze$ , the scan replacing sampling values of  $x_e$  with a single overall value for that line calculated by integration.

The above simplification due to quadrants symmetry applies also to any non-spherical form so long as it is symmetrical relative to the x-axis.

#### IV – X-SCAN INTEGRAL

##### Developing the Integrand

The quantity to be calculated is  $Avg[1/d^2]$ , by the accumulation of  $Incr$  [below] over the entire scan as follows.

$$AvgD_i = AvgD_{i-1} + Incr_i$$

$$Incr_i = \left[ \frac{x - \text{Component}}{\text{Particle Separation}} \right] \cdot \left[ \frac{\text{Inverse Square}}{\text{Separation}} \right]$$

$$Incr_i = \left( \frac{\Delta x}{d} \right) \cdot \left( \frac{1}{d^2} \right) \quad \Delta x \equiv [xs - xe + D] \quad \Delta y \equiv [ys - ye] \quad \Delta z \equiv [zs - ze]$$

$$d = \sqrt{\Delta x^2 + \Delta y^2 + \Delta z^2}$$

$$Incr_i = \left( \frac{xs - xe + D}{\sqrt{\Delta x^2 + \Delta y^2 + \Delta z^2}} \right) \cdot \left( \frac{1}{\Delta x^2 + \Delta y^2 + \Delta z^2} \right)$$

Define:  $X \equiv xs + D$        $Y \equiv \Delta y^2$        $Z \equiv \Delta z^2$

Therefore       $\Delta x = [X - xe]$

$$d = \sqrt{[X - xe]^2 + Y + Z}$$

$$Incr_i = \left( \frac{X - xe}{\sqrt{[X - xe]^2 + Y + Z}} \right) \cdot \left( \frac{1}{[X - xe]^2 + Y + Z} \right)$$

Let:       $x \equiv [X - xe]$        $K \equiv Y + Z$

Then:       $Incr_i = \frac{x}{[x^2 + K]^{3/2}}$

In terms of the variable of integration,  $x_e$ , [ $x$  below] and relative to its “encountered” origin the range of the  $x_e$  scan excursion is:

$$\text{from } -\sqrt{(Re^2 - ze^2)} - ye^2 \equiv -R \quad \text{to} \quad +\sqrt{(Re^2 - ze^2)} - ye^2 \equiv +R$$

but, the overall integration is in the source frame of reference and the range must so be. Therefore, the range is from  $[-R - D]$  to  $[+R - D]$ .

The integral is then:

$$\text{Incr} = \frac{1}{2 \cdot R} \cdot \int_{-R-D}^{+R-D} \frac{x}{[x^2 + K]^{\frac{3}{2}}} \cdot dx$$

where for scanning a single encountered x-line for a single source point [at  $z_s, y_s, x_s$ ] the encountered  $z_e$  and  $y_e$  are constants. The only variable is  $x_e$  as  $x$ .

The above derivation assumes the spheres case as in Figure 4-1; however, the same general procedure applies to any form having the same x-axis symmetry. The only modification needed is the range of the integration.

Evaluating the Integral

To integrate a function containing  $[x^2 + K]^{\frac{3}{2}}$  the procedure is to make the substitution:

$$x^2 + K = y^2 \quad \text{from which:} \quad x^2 = y^2 - K \quad \text{and:} \quad 2x \cdot dx = 2y \cdot dy.$$

The above integrand then transforms as follows:

$$\frac{x \cdot dx}{[x^2 + K]^{\frac{3}{2}}} = \frac{y \cdot dy}{y^3} = \frac{dy}{y^2}$$

The right hand expression of the integrand integrates as follows.

$$\int \frac{1}{y^2} \cdot dy = \int y^{-2} \cdot dy = \frac{y^{-1}}{-1} = -\frac{1}{y}$$

Reverting back through the substitution to a function of  $x$ :

$$\int \frac{x}{[x^2 + K]^{\frac{3}{2}}} \cdot dx = -\frac{1}{\sqrt{x^2 + K}}$$

But, this  $K = Y + Z = \Delta y^2 + \Delta z^2 = [y_s - y_e]^2 + [z_s - z_e]^2$  and is a constant relative to integrating on  $x$ .

Further  $x$  is  $[x_s - x_e + D]$  where  $x_e$  is the variable and  $x_s$  a constant; therefore:

$$\begin{aligned} \text{Incr} &= \frac{1}{2 \cdot R} \cdot \int_{-R+D}^{+R+D} \frac{x}{[x^2 + K]^{\frac{3}{2}}} \cdot dx = \frac{1}{2 \cdot R} \cdot \left[ -\frac{1}{\sqrt{x^2 + K}} \right] \begin{matrix} +R - D = +\sqrt{(Re^2 - ze^2) - ye^2} - D \\ -R - D = -\sqrt{(Re^2 - ze^2) - ye^2} - D \end{matrix} \\ &= \frac{1}{2 \cdot \sqrt{(Re^2 - ze^2) - ye^2}} \cdot \left[ -\frac{1}{\sqrt{[x_s - x_e + D]^2 + [y_s - y_e]^2 + [z_s - z_e]^2}} \right] \begin{matrix} +\sqrt{(Re^2 - ze^2) - ye^2} - D \\ -\sqrt{(Re^2 - ze^2) - ye^2} - D \end{matrix} \\ &= + \frac{1}{2 \cdot \sqrt{(Re^2 - ze^2) - ye^2}} \cdot \left[ -\frac{1}{\sqrt{[x_s - [ +\sqrt{(Re^2 - ze^2) - ye^2} - D] + D]^2 + [y_s - y_e]^2 + [z_s - z_e]^2}} \right. \\ &\quad \left. \dots \left[ x_s - \sqrt{(Re^2 - ze^2) - ye^2} + D + D \right]^2 \dots \right] \end{aligned}$$

$$\frac{1}{2 \cdot \sqrt{(Re^2 - ze^2) - ye^2}} \left[ \frac{1}{\sqrt{\left[ xs - \left[ -\sqrt{(Re^2 - ze^2) - ye^2} - D \right] + D \right]^2 + [ys - ye]^2 + [zs - ze]^2}} \right. \\ \left. \dots \left[ xs + \sqrt{(Re^2 - ze^2) - ye^2} + D + D \right]^2 \dots \right]$$

#### V – SCANNING AND CALCULATING THE X-SCAN INTEGRAL

The remaining procedure is to calculate the above evaluated integral in conjunction with scanning the  $M$  and  $m$  objects. Appendix 2 is a Basic Language program for performing the scanning and calculating the x-scan for each pair of particles selected.

#### APPENDICES [immediately following on next page]

- 1 – Summary of Tests Results
- 2 – A Sample Typical Basic Program File: Luther.bas .
- 3 – Comparison of Tests Parameters

Appendix 1 – Big G Calculation Tests Summary of Tests Results

Newton’s Law of Gravitation is  $a_g = G \cdot \frac{M}{d^2}$  That, with Law of Motion,  $F = m \cdot a$ , is  $F = [m] \cdot \left[ G \cdot \frac{M}{d^2} \right] = G \cdot \frac{M \cdot m}{d^2}$

Measurement = which experiment

D = spheres center-to-center separation distance

GR = General Relativity calculation of gravitation,  $1/d^2 = 1/D^2$

AvgD = Calculated average of parallel-to-centerline-components of reciprocal separation distances squared is  $1/d^2$ .

MN = Modern Newtonian calculation of gravitation using AvgD

Gm = reported measured *Big G*

Gc =  $Gm \cdot [GR/MN] = Gm \cdot [1/D^2 / AvgD]$

G from its relation to other fundamental constants =  $6.636,046,823 \times 10^{-11}$

SUMMARY OF TESTS RESULTS

All Data in SI Units: meters, kilograms, seconds

\* =  $\times 10^{-11}$

Measurement	Description of Experiment	Year	GR 1/D <sup>2</sup>	MN AvgD	Gm as * Measured	Corrected G *
Correct = 6.636,046,823						
Cavendish	Sphere on sphere torsion balance, deflection	1798	18.90	20.355,903,3	6.754	6.272
Rose	Sphere on cylinder, off-set by angular acceleration	1969	33.029,464,1	33.243,545,7	6.674	6.631
Luther	Sphere on torsion pendulum, oscillation frequency	1982	202.359,259,3	203.647,993,0	6.672,6	6.630,4
Bagley 1	Sphere on torsion pendulum, time-of-swing	1997	193.388,696,3	194.648,677,3	6.676,1	6.632,8
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Schlamminger	A Configuration of Cylinders, beam balance	2006	20.020,909,8	20.149,705,7	6.674,252	6.631,591
Quinn	Cylinders torsion pendulum, average of fixed deflection and period of oscillation	2013	0.138,195,9	0.139,108,2	6.675,66	6.631,67

Experiments Calculated

H. Cavendish, 1798, Wikipedia, “Cavendish Experiment”

R. Rose et al, 1969, “Determination of the Gravitational Constant G” PRL (21) 12.

G. Luther & W. Towler, 1982, “Redetermination of the Newtonian Gravitational Constant G” PRL (48) 3.

C. Bagley & G. Luther, 1997, “Preliminary Results of a Determination of the Newtonian Constant of gravitation: ...” PRL (78) 16.

J. Gundlach & S. Merkowitz, 2000, “Measurement of Newton’s Constant Using a Torsion Balance with Angular Acceleration Feedback”, PRL (85) 14.

St. Schlamminger et al, 2006, “Measurement of Newton’s Gravitational Constant”, Physical Review D of APS, **74**

T. Quinn *et al*, 2013, “Improved Determination of G Using Two Methods”, PRL **111**, 1011021 (2013)..

Experiments Not Calculated Because of Insufficient Dimensional Data

P. Heyl, 1930, “A Redetermination of the Constant of Gravitation”, NIST Archives.

P. Heyl & P. Chrzanowski, 1942, “A New Determination of the Constant of Gravitation”, NIST Archives.

M. Fitzgerald & T. Armstrong, 1995, IEEE Archives.

W. Michaelis *et al*, 1995, “A New Precise Determination of Newton’s Gravitational Constant”, Metrologia of IOP.

J. Schurr et al, 1998, “Gravitational Constant Measured by Means of a Beam Balance”, PRL of APS.

F. Nolting *et al*, 1999, “Determination of G by Means of a Beam Balance”, IEEE archives.

T. Armstrong & M. Fitzgerald, 2003, “New Measurement of G Using the Measurements Standards Laboratory’s Torsion Balance”, PRL of APS.



L. - C. Tu *et al*, 2010, “New Determination of the Gravitational Constant G with Time-of-Swing Method” Physical Review D of APS, **82** (022001) and J.Luo *et al*, 2009, “Determination of the Newtonian Gravitation Constant with Time of Swing Method”. PRL 102, 240801.

H. Parks & J. Fuller, 2010, “Simple Pendulum Determination of the Gravitational Constant”, PRL of APS.

*Appendix 2 - A Sample Typical Basic Program File: Luther.bas*

This program is a sample typical of the programs used for calculating the various experiments. It was prepared and run using the PowerBASIC Consol Compiler Integrated Development Environment (IDE) version 6.03 from PowerBASIC Inc.

```

FUNCTION PBMAIN
1 REM BIG G INTEGRATION CALCULATION BASIC PROGRAM
  CONSOLE.PRINT "METHOD = SPHERE TO SPHERE"
  CONSOLE.PRINT "EXPERIMENT = LUTHER"
  CONSOLE.PRINT ""
  CONSOLE.PRINT "START: DATE = "; DATE$, "  TIME = "; TIME$
  BD$ = DATE$
  BT$ = TIME$
10 REM OVERALL INITIALIZING
  DIM COUNT AS DOUBLE
  COUNT = 0
  DIM AVGD AS DOUBLE
  AVGD = 0
  DIM N AS DOUBLE
  N = 100
20 REM OVERALL INPUTTING
  DIM RS AS SINGLE
  DIM RE AS DOUBLE
  DIM SEPD AS DOUBLE
  DIM GM AS DOUBLE
  RS = 0.0508255
  RE = 0.0029
  SEPD = 0.07029727
  GM = 6.6726E-11
  DIM JS AS DOUBLE
  DIM JE AS DOUBLE
  JS = RS / N
  JE = JS / 10
30 REM INITIALIZE SOURCE SCAN - ZS CYCLE
  DIM ZSF AS DOUBLE
  ZSF = RS - JS / 2
  DIM ZS AS DOUBLE
  ZS = -JS/2
40 REM START NEXT SOURCE Z CYCLE
  ZS = ZS + JS
50 REM INITIALIZE SOURCE Y CYCLE
  DIM YSF AS DOUBLE
  YSF = (SQR(RS^2 - ZS^2))-JS/2
  DIM YS AS DOUBLE
  YS = -JS/2
55 REM DISPLAY
  IF COUNT > 0 THEN
    CONSOLE.PRINT "1 OVER SEPD^2 = "; 1 / (SEPD ^ 2), "AVGD = "; AVGD / COUNT
    CONSOLE.PRINT "ZS = "; ZS, " OUT OF ZSF = "; ZSF
    CONSOLE.PRINT " "
  END IF

```

```

60 REM START NEXT SOURCE Y CYCLE
  YS = YS + JS
70 REM INITIALIZE SOURCE X CYCLE
  DIM XSF AS DOUBLE
  XSF = (SQR(RS^2 - ZS^2 - YS^2))-JS/2
  DIM XS AS DOUBLE
  XS = -(SQR(RS^2 - ZS^2 - YS^2))-JS/2
80 REM START NEXT SOURCE X CYCLE
  XS = XS + JS
100 REM INITIALIZE ENCOUNTERED SCAN - ZE CYCLE
  DIM ZEF AS DOUBLE
  ZEF = RE - JE / 2
  DIM ZE AS DOUBLE
  ZE = -JE/2
110 REM START NEXT ENCOUNTERED Z CYCLE
  ZE = ZE + JE
120 REM INITIALIZE ENCOUNTERED Y CYCLE
  DIM YEF AS DOUBLE
  YEF = (SQR(RE^2 - ZE^2))-JE/2
  DIM YE AS DOUBLE
  YE = -JE/2
130 REM START NEXT ENCOUNTERED Y CYCLE
  YE = YE + JE
170 REM XE CALCULATION BY FORMULA
  DIM CUMINCR AS DOUBLE
  CUMINCR = 0
  DIM RAD AS DOUBLE
  RAD = (RE ^ 2 - ZE ^ 2)
  IF RAD > YE ^ 2 THEN
    RAD = SQR(RAD - YE ^ 2)
  ELSE
    RAD = 0
    GOTO 200
  END IF
  DIM TAIL AS DOUBLE
  TAIL = XS + SEPD + SEPD
  DIM BALNC AS DOUBLE
  BALNC = (YS - YE) ^ 2 + (ZS - ZE) ^ 2
  DIM FIRST AS DOUBLE
  FIRST = 1 / (2 * RAD)
  DIM PIECEA AS DOUBLE
  PIECEA = (RAD + TAIL) ^ 2
  DIM SECOND AS DOUBLE
  SECOND = 1 / SQR(PIECEA + BALNC)
  DIM PIECEB AS DOUBLE
  PIECEB = (-RAD + TAIL) ^ 2
  DIM THIRD AS DOUBLE
  THIRD = 1 / SQR(PIECEB + BALNC)
  DIM CHG AS DOUBLE
  CHG = ABS(FIRST * (THIRD - SECOND))
  CUMINCR = CUMINCR + CHG

```

```

BALNC = (-YS - YE) ^ 2 + (ZS - ZE) ^ 2
SECOND = 1 / SQR(PIECEA + BALNC)
THIRD = 1 / SQR(PIECEB + BALNC)
CHG = ABS(FIRST * (THIRD - SECOND))
CUMINCR = CUMINCR + CHG + CHG
BALNC = (-YS - YE) ^ 2 + (-ZS - ZE) ^ 2
SECOND = 1 / SQR(PIECEA + BALNC)
THIRD = 1 / SQR(PIECEB + BALNC)
CHG = ABS(FIRST * (THIRD - SECOND))
CUMINCR = CUMINCR + CHG
AVGD = AVGD + CUMINCR
COUNT = COUNT + 1
200 REM LOGIC FOR YE SCAN
    IF YE < YEF THEN
        GOTO 130
    END IF
202 REM EC FOR YE OVERRUN
    DIM FRACT AS DOUBLE
    FRACT = (YE - YEF)/JE
    CHG = CUMINCR*FRACT
    AVGD = AVGD - CHG
204 REM LOGIC FOR ZE SCAN
    IF (ABS(ZE)) < ZEF THEN
        GOTO 110
    END IF
210 REM LOGIC FOR XS SCAN
    IF (ABS(XS)) < XSF THEN
        GOTO 80
    END IF
214 REM LOGIC FOR YS SCAN
    IF (ABS(YS)) < YSF THEN
        GOTO 60
    END IF
218 REM LOGIC FOR ZS SCAN
    IF (ABS(ZS)) < ZSF THEN
        GOTO 40
    END IF
230 REM FINAL RESULTS
    AVGD = AVGD / COUNT
    DIM WRONGD AS DOUBLE
    WRONGD = 1 / SEPD ^ 2
    DIM RATIO AS DOUBLE
    RATIO = WRONGD / AVGD
    DIM CORRECTG AS DOUBLE
    CORRECTG = RATIO * GM
240 REM RESULTS DISPLAY
    XPRINT ATTACH DEFAULT
    XPRINT "METHOD = SPHERE TO SPHERE"
    XPRINT "EXPERIMENT = ROSE"
    XPRINT ""
    XPRINT "RS = "; RS

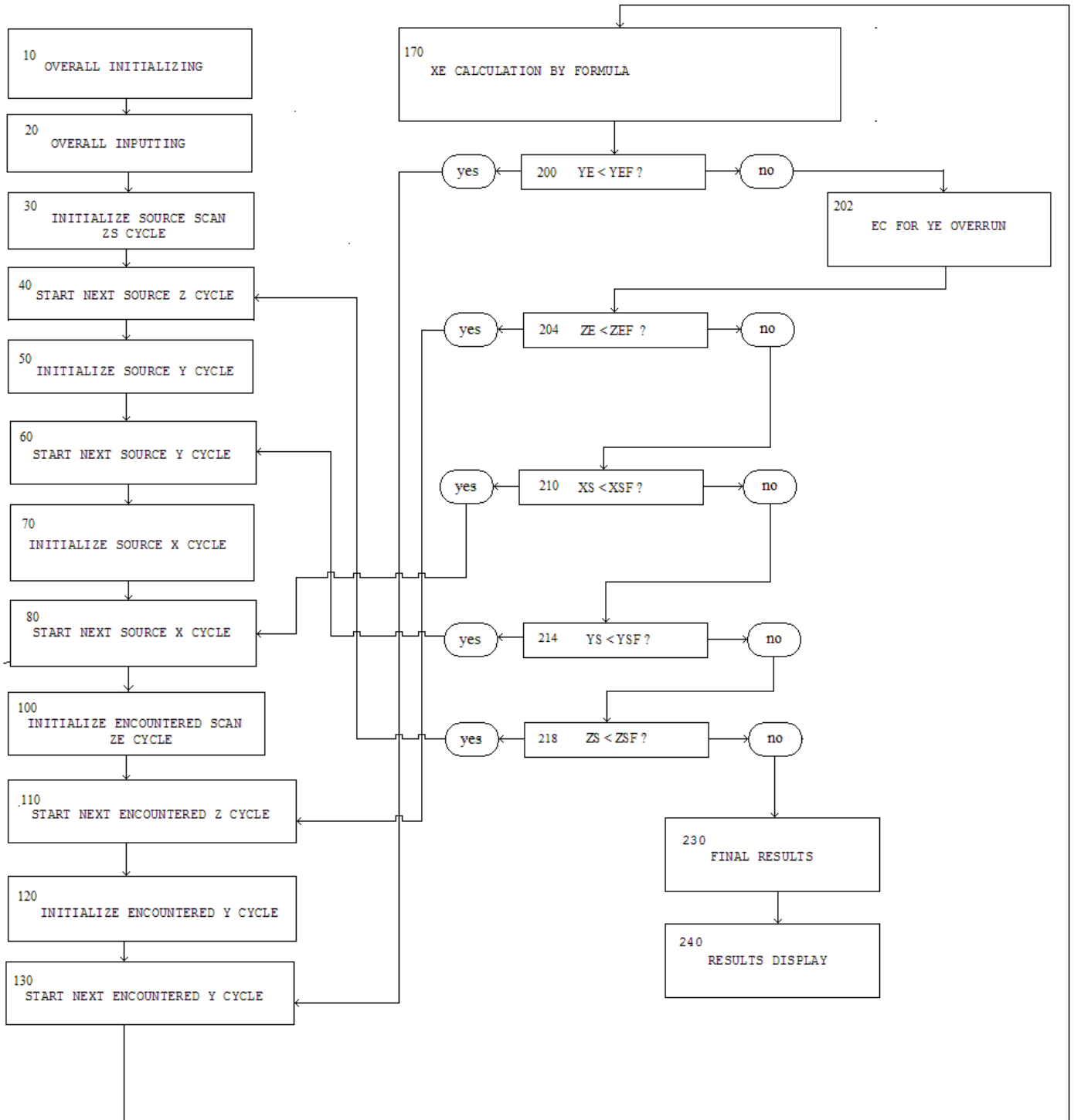
```

```

XPRINT "RE = "; RE
XPRINT "SEPD = "; SEPD
XPRINT "GM = "; GM
XPRINT "GR = GENERAL RELATIVITY   MN = MODERN NEWTON"
XPRINT ""
XPRINT "N = "; N
XPRINT "GR RECIPROCAL SQUARED X-COMPONENT DISTANCE = "; WRONGD
XPRINT "MN RECIPROCAL SQUARED X-COMPONENT DISTANCE = "; AVGD
XPRINT ""
XPRINT "RATIO GR/MN = "; RATIO
XPRINT ""
XPRINT "CORRECTED G = "; CORRECTG
XPRINT "FORMULA G = "+ STR$(6.636046823E-11)
XPRINT ""
CONSOLE.PRINT "GR = GENERAL RELATIVITY   MN = MODERN NEWTON"
CONSOLE.PRINT ""
CONSOLE.PRINT "N = "; N
CONSOLE.PRINT "GR RECIPROCAL SQUARED X-COMPONENT DISTANCE = "; WRONGD
CONSOLE.PRINT "MN RECIPROCAL SQUARED X-COMPONENT DISTANCE = "; AVGD
CONSOLE.PRINT ""
CONSOLE.PRINT "RATIO GR/MN = "; RATIO
CONSOLE.PRINT ""
CONSOLE.PRINT "CORRECTED G = "; CORRECTG
CONSOLE.PRINT ""
FT$ = TIMES$
FD$ = DATES$
XPRINT "START DATE WAS "; BD$; "   FINISH DATE WAS "; FD$
XPRINT "START TIME WAS "; BT$; "   FINISH TIME WAS "; FT$
XPRINT CLOSE
CONSOLE.WAITSTAT
END FUNCTION

```

BIG G CALCULATION BASIC FLOW DIAGRAM



## Appendix 3 – Comparison of Parameters

Appendix 3 – Comparison of Parameters

Test	Variable	Per Experiment Published Paper		As These Calculations Run	
		Notes	Value	Value	Notes
Rose	Rs	Large attraction less small repulsion +/- due to spheres acting on each side of small narrow rod- pendulum to net fixed deflection.	0.0508	0.0508	Per mathcad equivalent sphere. Per narrow rod pendulum +/- effect.
	Re		Equivalent Sphere <sup>1</sup>	0.0066	
	SepD		0.12	0.174	
Luther	Rs	Pendulum oscillates therefore SepD varies with pendulum oscillation.	0.0508255	0.0508255	Per mathcad equivalent sphere.
	Re		Equivalent Sphere	0.0029	
	SepD		0.07029727	0.07029727	
Bagley 1	Rs	Partially same set-up as in Luther	0.0508255	0.0508255	Per mathcad equivalent sphere.
	Re		Equivalent Sphere	0.0029	
	SepD		0.0719092	0.0719092	
Bagley 2	Rs	Partially same set-up as in Luther	0.0508255	0.0508255	Per mathcad equivalent sphere.
	Re		Equivalent Sphere	0.0029	
	SepD		0.0698567	0.0698567	
Gundlach	Rs	Large attraction less small repulsion +/- due to spheres acting on each side of flat thin pendulum to net fixed deflection.	0.06245	0.06245	Per mathcad equivalent sphere.
	Re		Equivalent Sphere	0.0104	
	SepD		Anomalous	0.2575 *	
Schlamminger	Rs	Approximately half of the small encountered cylinder overlaps the larger by being inside at one end of its central cavity. Thus SepD is indeterminate as is the point-on-point action there.	0.7	0.7	Evaluated to compensate overlap.
	Le		0.077	0.077	
	Rs		0.523	0.523	
	Ri		0.050	0.050	
	Re		0.0225	0.02215	
	SepD		0.3465	0.22349	
Quinn	Rs	1. Test cylinders oscillate therefore SepD varies with oscillation. 2. Large attraction less smaller repulsion +/- due to source cylinders acting opposite, and at an angle on each side of, test cylinder.	0.115	0.115	Per "Notes" column 3 and below.
	Le		0.055	0.055	
	Rs		0.060	0.060	
	Re		0.0275	0.0275	
	SepD		0.214	2.690	

Appendix 3 – Comparison of Parameters [continued]

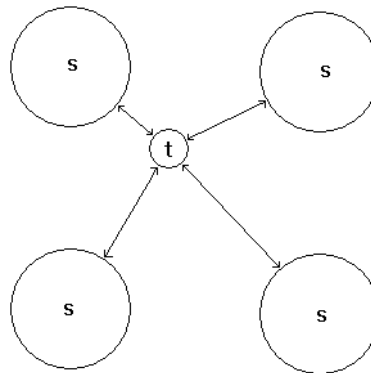
In above table all dimensions in meters.

[1] Equivalent sphere is a sphere of the same total volume as the actual encountered test mass [and therefore it has the same number of interacting particles as the actual] and, to the extent possible, located with its center at the encountered test mass end of the actual SepD [producing the same average separation].

NOTES re QUINN

In the Quinn experiment 4 larger field masses confront 4 smaller test masses as in the Figure below.

Multiple Sources on One Test Effect



All four sources shown.  
Only one of four tests shown  
at test deflection angle.

Cylinders seen from above.

Because the modeling for the MODERN NEWTONIAN Calculation is of one field mass acting on one test mass the model incorporates only the upper left field [source] mass. the effect of the other 3 field masses and of the other 3 test masses, not shown, is to oppose, that is to reduce, the overall gravitational effect of the upper left field mass on its test mass.

The model of only one field mass accounts for that by a much greater value of SepD for the calculations.

Having contended that the theory of gravitation set forth in Einstein’s “General Theory of Relativity” is wrong and unacceptable because there is no supporting mechanism by which its contended “curving of space” can occur or be caused, it is incumbent upon the present author to provide an alternative theory.

That is the function of the next Section 6





